

## Effect of Temperature on the Aqueous Two-Phase System Containing Poly(ethylene glycol) Dimethyl Ether 2000 and Dipotassium Oxalate

Mohammed Taghi Zafarani-Moattar\* and Vahid Hosseinpour-Hashemi

Physical Chemistry Department, University of Tabriz, Tabriz 51664, Iran

The Effective excluded volumes, EEV; and the free energy changes,  $\Delta G_c$ , for clouding point of PEGDME2000 +  $K_2C_2O_4$  + water system

$T/K$	$EEV$ (g . mol <sup>-1</sup> )	$\Delta G_c$ (kJ . mol <sup>-1</sup> )
298.15	25.7619	-12.294
303.15	26.3481	-12.666
308.15	26.8673	-13.040
318.15	28.4141	-13.837

The EEV values.

$\Delta G_c$  values

PHASE SEPARATION ABILITY INCREASED BY INCREASING THE TEMPERATURE.

**ABSTRACT:** Liquid–liquid equilibria (LLE) of the poly(ethylene glycol) dimethyl ether 2000 (PEGDME2000) + dipotassium oxalate +  $H_2O$  system have been determined experimentally at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15)$  K. The effect of temperature on the binodal curves and tie-lines has also been studied. The Graber et al., Merchuk, and empirical equations were used to correlate the binodal data of this system with the temperature dependence expressed in the linear form with  $(T - T_0)$  K as a variable. Furthermore, we used the Othmer–Tobias and Bancroft and a temperature-dependent Setschenow-type equation for the correlation and prediction of the liquid–liquid phase behavior of the studied system. The effective excluded volume (EEV) values obtained from the binodal model for this system and other aqueous PEGDME2000–salt systems were determined, and the relation between these values and salting-out ability of different salts was discussed. Also, the effects of type of the polymers PEGDME2000 and PEG2000 on LLE are discussed. Finally, the free energies of cloud points for this system were calculated. According to the results it was concluded that the increase of the entropy is a driving force for the formation of the studied aqueous two-phase system (ATPS).

### 1. INTRODUCTION

The aqueous two-phase system (ATPS) presents a powerful technique for the separation of the biological materials. There are two kinds of ATPS's: the polymer–polymer ATPS and the polymer–salt ATPS; the latter has more advantages. These systems, introduced in 1965 by the pioneering work of Albertsson, have been applied in the separation of biological materials, such as proteins, enzymes, and nucleic acids.<sup>1–3</sup>

Zaslavsky presented a useful summary of experimental liquid–liquid data and equilibrium (LLE) diagrams for systems formed by poly(ethylene glycol) (PEG), inorganic salts, and water.<sup>3</sup> Poly(ethylene glycol) dimethyl ether 2000 (PEGDME2000) is another polymer that has a similar structure to the PEG. Thus, PEGDME can be used to form ATPS's with kosmotropic (i.e., water structure) salts. As far as we know there are few experimental LLE data for ATPS's with this polymer.<sup>4–8</sup>

In this work, the phase diagrams have been determined for ATPS's containing PEGDME2000 and dipotassium oxalate ( $K_2C_2O_4$ ) at  $T = (298.15, 318.15, \text{ and } 318.15)$  K. There are no experimental liquid–liquid data in the literature for this system.

The advantage of using oxalate is that it is biodegradable and therefore it could be discharged into biological wastewater plants in the separation of biological materials. Furthermore, plait points of system have been calculated in each temperature using linear least-squares regression method, and based on cloud point values the free energies of the clouding process have been estimated. In addition, the effective excluded volume (EEV) values obtained from the binodal model<sup>9</sup> for this system at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15)$  K have been used to study the effect of temperature on the phase-forming ability of the investigated system. The EEV values for the other previously studied PEGDME2000 + salt + water systems<sup>6,8</sup> were also calculated, and obtained values were used to compare the salting-out ability of different salts in these systems. On the basis of the Gibbs free energy of hydration of salts, the relations between these values and salting-out ability of different salts were also discussed. Also the effect of the polymers

Received: October 12, 2011

Accepted: December 21, 2011

Published: January 10, 2012

PEGDME2000 and PEG2000 on the phase-forming ability of these two-phase systems containing dipotassium oxalate was studied. The effect of temperature on the tie-lines was also studied.

An empirical equation<sup>6</sup> and the Graber et al.<sup>10</sup> and the Merchuk<sup>11</sup> equations as a function of temperature were used for the correlation of binodal data and the prediction of them at  $T = 303.15$  K and compared with experimental data. The Othmer–Tobias and Bancroft<sup>12</sup> and Setschenow-type<sup>13</sup> equations have been used to correlate the experimental LLE data of investigated ATPS's. Likewise, the Setschenow-type equation<sup>13</sup> has also been used for the prediction of tie-line data at  $T = 303.15$  K.

## 2. MATERIALS AND METHODS

**2.1. Materials.** PEGDME2000 with CAS Registry No. 24991-55-7 and PEG2000 with CAS Registry No. 25322-68-3 were obtained from Merck. The number average molar mass of the polymer was previously determined to be  $2305 \text{ g}\cdot\text{mol}^{-1}$ , using gel permeation chromatography (GPC, Agilent, USA).<sup>4</sup> Dipotassium oxalate monohydrate ( $\text{K}_2\text{C}_2\text{O}_4\cdot\text{H}_2\text{O}$ ) with CAS Registry No. 6487-48-5 with a minimum mass fraction purity of 99 % was obtained from Merck. The polymers and salt were used without further purification, and double-distilled deionized water was used.

**2.2. Apparatus and Procedure.** The experimental apparatus employed is essentially similar to the one used in previous works.<sup>4,5</sup> The binodal curves were determined by clouding point titration method.<sup>4</sup> In this method the temperature was controlled using a thermostat (HETO BIRKERØD, type: 01 TE 623, Denmark) within  $\pm 0.05$  K. The composition of the mixture for each point on the binodal curve was calculated by mass using an analytical balance (Shimadzu, 321-34553, Shimadzu Co., Japan) with a precision of  $\pm 1\cdot 10^{-7}$  kg. The maximum uncertainty was found to be  $\pm 0.002$  in determining the mass fraction of both polymers and salt by using this method.

For the determination of the tie-lines, feed samples (about  $2\cdot 10^{-5} \text{ m}^3$ ) were prepared by mixing appropriate amounts of polymer, salt, and water in the vessel. The samples were stirred for 1 h and then placed in the thermostatted bath. The temperature of the thermostatted bath was controlled using a thermostat (JULABO model MB, Germany) with an accuracy of  $\pm 0.02$  K and allowed to settle for at least 48 h to separate into two clear phases. After separations of the two phases, the concentrations of dipotassium oxalate in the top and bottom phases were determined by flame photometry (Jenway PFP7, England). In this method, first we prepared about 11 standard solutions having the potassium ion in the concentration ranges of (150 to 250) ppm. Then, using these standard solutions the flame photometer has been calibrated. To measure potassium concentration in the samples taken from the top and bottom phases, it was necessary to dilute these solutions to place in the ranges of (150 to 250) ppm. The concentrations of samples were determined using obtained absorption values and the calibration curve. The maximum uncertainty was found to be  $\pm 0.002$  in determining the mass fraction of salt by using this method. The concentration of PEGDME in both phases was determined by refractive index measurements performed at  $T = 298.15$  K using a refractometer (Atago DR-A<sub>1</sub>, Japan) with a precision of  $\pm 0.0001$ . The uncertainty in refractive index measurement is  $\pm 0.0002$ . For dilute aqueous solutions containing a polymer and a salt, the relation between the

refractive index,  $n_D$ , and the mass fractions of polymer,  $w_p$ , and salt,  $w_s$  is given by<sup>14</sup>

$$n_D = n_0 + a_p w_p + a_s w_s \quad (1)$$

where  $n_0$  is the refractive index of pure water which is set to 1.3325 at  $T = 298.15$  K.  $a_p$  and  $a_s$  are constants of the polymer and salt, respectively, for which linear calibration plots of the refractive index of the solution are obtained. However, it should be noted that eq 1 is only valid for dilute solutions. Therefore, it was necessary to dilute the samples before refractive index measurements, to be in the mass fraction range ( $C$  range) presented in Table 1. The uncertainty of the mass fraction of

**Table 1. Values of the Parameters of Equation 1,  $a_i$ , for the PEGDME2000 (p) +  $\text{K}_2\text{C}_2\text{O}_4$  (s) +  $\text{H}_2\text{O}$  (w) System**

material	constant	value	C range (w/w)	$R^2$ <sup>a</sup>
PEGDME2000	$a_p$	0.1358	0–0.15	0.9999
$\text{K}_2\text{C}_2\text{O}_4$	$a_s$	0.1373	0–0.12	0.9999

<sup>a</sup> $R^2$  represents the respective correlation coefficient value of the linear calibration plot of the refractive index against the mass fraction for PEGDME2000 or  $\text{K}_2\text{C}_2\text{O}_4$  at the mass fraction range ( $C$  range) of each material.

PEGDME achieved using eq 1 was better than 0.002. The values of these constants and respective correlation coefficient values,  $R^2$ , are given in Table 1.

## 3. RESULTS AND DISCUSSION

**3.1. Experimental Results.** For the PEGDME2000 + dipotassium oxalate + water system the experimental binodal data and the tie-line compositions at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15)$  K are given in Tables 2 and 3, respectively.

**Table 2. Experimental Binodal Data in Mass Fraction,  $w_i$ , for the PEGDME2000 (p) +  $\text{K}_2\text{C}_2\text{O}_4$  (s) +  $\text{H}_2\text{O}$  (w) System at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15)$  K**

$T/K = 298.15$		$T/K = 303.15$		$T/K = 308.15$		$T/K = 318.15$	
$100w_p$	$100w_s$	$100w_p$	$100w_s$	$100w_p$	$100w_s$	$100w_p$	$100w_s$
39.23	4.45	40.49	4.06	41.20	3.77	42.41	3.22
38.58	4.54	39.67	4.16	40.06	3.91	41.88	3.27
37.64	4.68	38.87	4.27	39.29	4.00	40.91	3.37
36.74	4.81	37.80	4.42	38.33	4.13	40.00	3.47
35.40	5.02	36.75	4.58	37.43	4.26	38.86	3.61
34.18	5.21	35.20	4.82	36.11	4.47	36.00	4.00
32.51	5.53	33.85	5.04	34.86	4.66	34.49	4.21
31.01	5.82	31.95	5.39	33.17	4.96	32.37	4.55
29.11	6.23	30.38	5.70	31.66	5.24	30.62	4.85
27.51	6.62	28.41	6.12	29.66	5.63	28.32	5.28
25.56	7.11	26.75	6.51	27.90	6.02	26.43	5.67
23.94	7.57	24.78	7.01	25.92	6.49	24.02	6.23
22.09	8.12	23.13	7.47	24.28	6.90	22.14	6.70
20.58	8.62	21.30	8.04	22.39	7.43	20.18	7.25
18.94	9.21	19.78	8.53	20.87	7.89	16.76	8.21
17.62	9.68	18.14	9.10	19.19	8.42	15.45	8.62
16.07	10.28	16.70	9.62	17.79	8.90		
				16.17	9.42		

**3.1.1. Effect of Temperature.** The effect of temperature on the phase-forming ability in the studied system is also shown in Figure 1. The locus for the experimental binodals shown in Figure 1 indicates that the two-phase area is expanded with an

**Table 3. Experimental Tie-Lines Data in Mass Fraction,  $w_p$ , for the PEGDME2000 (p) +  $K_2C_2O_4$  (s) +  $H_2O$  (w) System at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15)$  K together with Tie-Line Length, TLL, and Slope, S**

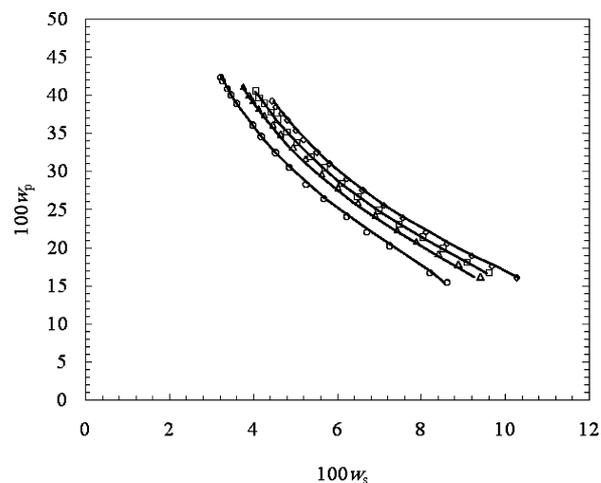
feed sample <sup>a</sup>		top phase		bottom phase		S	TLL
$100w'_p$	$100w'_s$	$100w_p$	$100w_s$	$100w_p$	$100w_s$		
$T/K = 298.15$							
18.00	10.00	24.53	7.39	2.72	16.08	-2.51	23.48
18.02	11.01	30.78	5.80	1.31	17.96	-2.42	31.87
17.96	11.99	34.26	5.13	0.59	19.19	-2.39	36.49
17.99	13.02	37.72	4.65	0.23	20.75	-2.33	40.81
18.03	14.00	39.88	4.28	0.23	22.02	-2.24	43.44
18.02	15.03	43.17	3.90	0.16	23.31	-2.22	47.19
18.00	16.01	45.54	3.71	0.12	24.04	-2.23	49.76
$T/K = 303.15$							
18.01	10.00	26.58	6.57	2.13	16.43	-2.48	26.36
18.03	11.02	31.06	5.65	1.61	17.64	-2.46	31.80
18.01	12.00	35.24	4.87	0.65	19.07	-2.44	37.40
18.01	13.02	38.67	4.25	0.57	20.42	-2.36	41.39
18.03	13.99	41.90	3.93	0.47	21.86	-2.31	45.15
18.02	15.01	44.35	3.65	0.44	22.87	-2.28	47.93
18.04	15.99	46.96	3.41	0.33	23.83	-2.28	50.90
$T/K = 308.15$							
18.03	10.00	27.66	6.09	2.13	16.57	-2.44	27.60
18.02	11.01	32.02	5.21	0.91	18.12	-2.41	33.68
18.00	12.00	35.82	4.56	0.37	19.39	-2.39	38.43
18.04	13.01	38.60	4.14	0.31	20.69	-2.31	41.72
17.76	13.80	40.54	3.86	0.18	21.49	-2.29	44.05
18.03	15.01	43.71	3.59	0.13	22.79	-2.27	47.62
18.03	15.80	45.77	3.47	0.09	24.10	-2.21	50.13
$T/K = 318.15$							
18.00	10.00	33.17	4.37	0.52	16.72	-2.64	34.91
18.00	11.01	36.63	3.93	0.37	18.06	-2.57	38.91
18.06	12.00	39.00	3.69	0.29	19.33	-2.48	41.75
17.99	12.98	42.28	3.21	0.25	20.06	-2.49	45.28
18.03	14.00	44.22	3.00	0.18	21.47	-2.38	47.75
18.04	15.00	46.78	2.88	0.15	22.69	-2.35	50.67
18.03	16.00	48.92	2.71	0.11	23.92	-2.30	53.22

<sup>a</sup> $w'_p$  and  $w'_s$  are the total mass fractions of polymer and salt in its feed samples, respectively.

increase in temperature. The effect of temperature on the obtained binodals can be explained using the binodal model.<sup>9</sup> This model is based on the statistical geometry methods from which the EEV can be determined. It was found that bigger EEV values correspond to a higher salting-out ability of salt in polymer + salt + water systems.<sup>9</sup> The binodal equation for the aqueous polymer–salt systems can be written as

$$\ln\left(V_{123}^* \frac{w_p}{M_p}\right) + V_{123}^* \frac{w_s}{M_s} = 0 \quad (2)$$

where  $V_{123}^*$  is the EEV.  $M_p$  and  $M_s$  are the molar mass of polymer and salt, respectively. The EEV values obtained from the correlation of binodal data of investigated systems at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15)$  K along with the corresponding standard deviations (SD) are given in Table 4. The correlation coefficient values and the small standard deviations reported in Table 4 indicate that the binodal model<sup>9</sup> represents the obtained binodal data for the PEGDME2000 +  $K_2C_2O_4$  +  $H_2O$  system with excellent accuracy at different working temperatures. Also as can be seen from Table 4, EEV



**Figure 1.** Plot of the mass fraction of polymer against the mass fraction of salt to show binodal curves for the PEGDME2000 (p) +  $K_2C_2O_4$  (s) + water (w) two-phase system at different temperatures:  $\diamond$ ,  $T = 298.15$ ;  $\square$ ,  $T = 303.15$ ;  $\triangle$ ,  $T = 308.15$  and  $\circ$ ,  $T = 318.15$ , and (solid line) calculated from eq 5.

**Table 4. Effective Excluded Volumes, EEV ( $g \cdot mol^{-1}$ ), as Determined by the Regression of the Statistical Geometry Model<sup>9</sup> for PEGDME2000 +  $K_2C_2O_4$  +  $H_2O$  at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15)$  K**

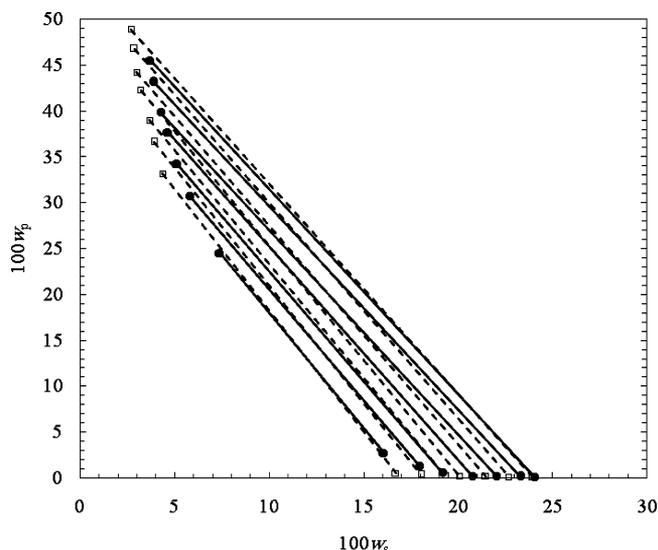
T/K	EEV	$R^2$	SD <sup>a</sup>
298.15	25.7619	0.9990	0.02
303.15	26.3481	0.9989	0.00
308.15	26.8673	0.9994	0.01
318.15	28.4141	0.9993	0.09

<sup>a</sup>SD =  $(\sum_{i=1}^N (100w_s^{cal} - 100w_s^{exp})^2 / N)^{0.5}$ , where  $N$  represents the number of binodal data, respectively.

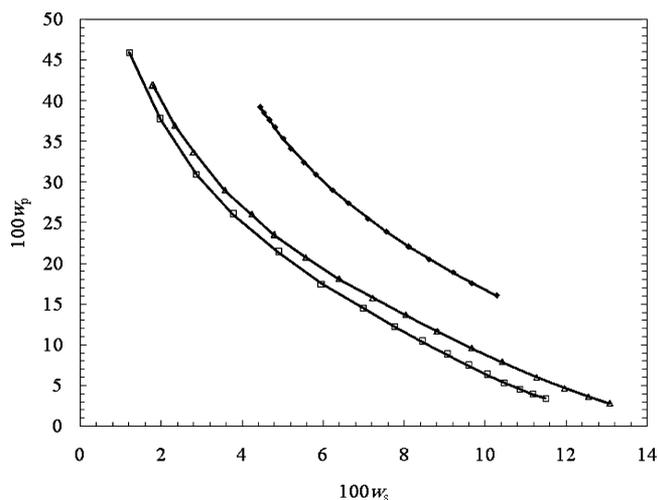
values are increased by increasing the temperature. This means that the salting-out ability of the studied system is increased by increasing the temperature.

To show the effect of temperature on the equilibrium phase compositions for the investigated system, the experimental tie-lines are compared in Figure 2, for the temperatures  $T = (298.15 \text{ and } 318.15)$  K. As shown in Figure 2, the slope and the length of the tie-lines increased with an increase in temperature. In other words, the concentration of salt in the bottom phase which is in equilibrium with a certain concentration of PEGDME in the top phase decreases by increasing temperature. This is because the PEGDME2000 becomes more hydrophobic with an increase in temperature.<sup>15</sup> Thus, by increasing temperature, water is driven from the polymer-rich phase to the salt-rich phase, so the polymer concentration at the polymer-rich phase increases, while the salt-rich phase will be somewhat more diluted (i.e., the salt concentration will be decreased).

**3.1.2. Effect of Salt.** To see the effectiveness of the anion in forming an ATPS with PEGDME, the experimental binodal curves of the {PEGDME2000 +  $K_2C_2O_4$  +  $H_2O$ }, {PEGDME2000 +  $K_3PO_4$  +  $H_2O$ }, and {PEGDME2000 +  $K_2HPO_4$  +  $H_2O$ } systems<sup>6,8</sup> are shown in Figure 3 at  $T = 298.15$  K. In Figure 3, considering that the salts have a common cation but contain different anions, it is easy to see that the salting-out ability of the anions follows the ordering  $PO_4^{3-} > HPO_4^{3-} > C_2O_4^{2-}$ . The salting-out ability can also be related to the Gibbs free energy of hydration of ions ( $\Delta G_{hyd}$ ). For  $PO_4^{3-}$ ,



**Figure 2.** Plot of the mass fraction of polymer against the mass fraction of salt to illustrate the effect of temperature on the slope and length of tie-lines of the {PEGDME2000 (p) +  $\text{K}_2\text{C}_2\text{O}_4$  (s) +  $\text{H}_2\text{O}$  (w)} system:  $\bullet$ ,  $T = 298.15$  K;  $\square$ ,  $T = 318.15$  K; —, tie-lines at 298.15 K; - - -, tie-lines at 318.15 K. Tie-lines were obtained by connecting the experimental equilibrium phase composition data.



**Figure 3.** Binodal curves for the {PEGDME2000 (p) + salt (s) +  $\text{H}_2\text{O}$  (w)} systems at  $T = 298.15$  K.  $\blacklozenge$ ,  $\text{K}_2\text{C}_2\text{O}_4$ ;  $\triangle$ ,  $\text{K}_2\text{HPO}_4$ ;  $\square$ ,  $\text{K}_3\text{PO}_4$ .

the  $\Delta G_{\text{hyd}} = -2835 \text{ kJ}\cdot\text{mol}^{-1}$  has been reported by Marcus.<sup>16</sup> For the anions  $\text{HPO}_4^{2-}$  and  $\text{C}_2\text{O}_4^{2-}$ , Zafarani-Moattar and Zaferanloo<sup>17</sup> estimated the  $\Delta G_{\text{hyd}}$  values respectively ( $-1789$  and  $-1577$ )  $\text{kJ}\cdot\text{mol}^{-1}$ , using the procedure given by Marcus.<sup>16</sup> Therefore, it seems that better salting-out of PEGDME is observed when the anions of the salt have a more negative  $\Delta G_{\text{hyd}}$  value. For studying the effect of salts on the salting-out ability in PEGDME2000 + salt + water systems, the binodal model<sup>9</sup> can also be used. Using the experimental binodal obtained in this work and other published data,<sup>6,8</sup> the EEV values were determined at  $T = 298.15$  K by eq 2 for these systems and are collected in Table 5. The increase of EEV values in the order  $\text{K}_3\text{PO}_4 > \text{K}_2\text{HPO}_4 > \text{K}_2\text{C}_2\text{O}_4$  indicates the same order of salting-out ability of these salts in the PEGDME2000 + salt + water systems. This trend is also evident from Figure 3.

**Table 5.** Comparison of Free Energies of Hydration for Anions,  $\Delta G_{\text{hyd}}$  ( $\text{kJ}\cdot\text{mol}^{-1}$ ), and Effective Excluded Volumes, EEV ( $\text{g}\cdot\text{mol}^{-1}$ ), for PEGDME2000 + Salt + Water Systems at  $T = 298.15$  K

salt	$\Delta G_{\text{hyd}}$	EEV	$R^2$	SD
$\text{K}_2\text{C}_2\text{O}_4$	-1577	25.7619	0.9990	0.02
$\text{K}_2\text{HPO}_4$	-1789	34.8344	0.9744	0.61
$\text{K}_3\text{PO}_4$	-2835	42.0717	0.9786	0.99

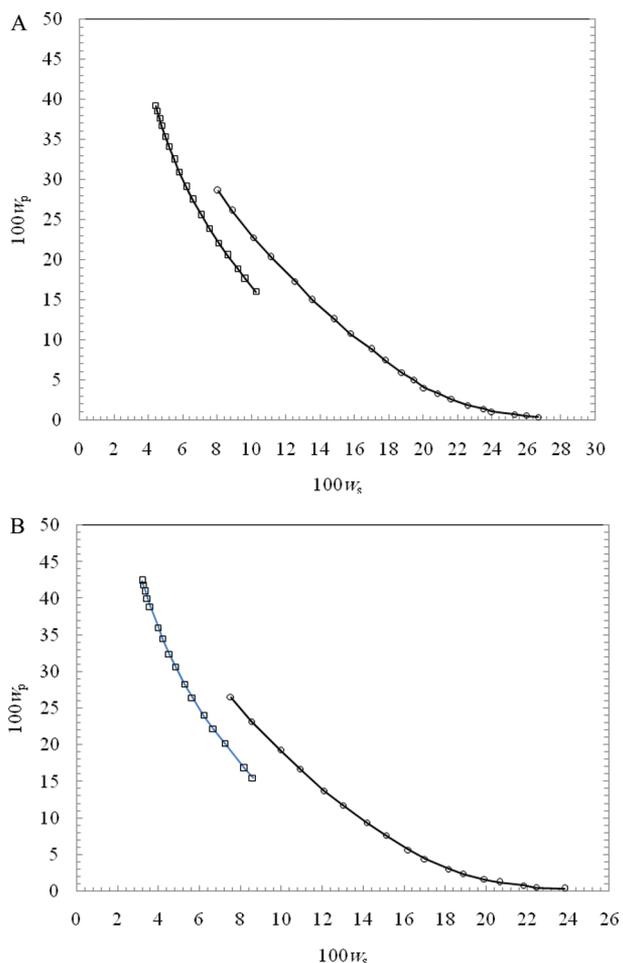
**3.1.3. Effect of the Polymer.** PEGDME has a similar structure to PEG. In this regard, our interest lies in comparison of the phase-forming ability of these polymers. To accomplish this, we decided to determine the binodal curve of the system (PEG2000 +  $\text{K}_2\text{C}_2\text{O}_4$  +  $\text{H}_2\text{O}$ ) using PEG with the same molar mass of  $2000 \text{ g}\cdot\text{mol}^{-1}$  for which there are no experimental binodal data in the literature. We determined binodals for the PEG2000 +  $\text{K}_2\text{C}_2\text{O}_4$  +  $\text{H}_2\text{O}$  system at  $T = (298.15 \text{ and } 318.15)$  K, and the binodal data are given in Table 6; and the

**Table 6.** Experimental Binodal Data in Mass Fraction,  $w_i$ , for the PEGDME2000 (p) +  $\text{K}_2\text{C}_2\text{O}_4$  (s) +  $\text{H}_2\text{O}$  (w) System at  $T = (298.15 \text{ and } 318.15)$  K

$T/\text{K} = 298.15$		$T/\text{K} = 318.15$	
$100w_p$	$100w_s$	$100w_p$	$100w_s$
28.64	8.08	26.50	7.54
26.14	8.89	23.22	8.54
22.82	10.12	19.30	9.98
20.34	11.15	16.71	10.91
17.35	12.53	13.71	12.07
15.01	13.55	11.71	13.02
12.61	14.83	9.32	14.19
10.83	15.77	7.59	15.13
8.86	17.01	5.64	16.22
7.54	17.78	4.41	17.02
5.94	18.78	3.05	18.17
5.05	19.43	2.34	18.89
4.08	20.05	1.60	19.93
3.39	20.84	1.21	20.66
2.64	21.65	0.80	21.84
1.91	22.57	0.49	22.44
1.44	23.50	0.34	23.84
1.12	24.00		
0.78	25.30		
0.60	25.99		
0.39	26.67		

corresponding binodal curves together with the binodal curves for (PEGDME<sub>2000</sub> +  $\text{K}_2\text{C}_2\text{O}_4$  +  $\text{H}_2\text{O}$ ) are shown in Figure 4a,b, at  $T = (298.15 \text{ and } 318.15)$  K, respectively. Considering that both of the polymers have the same molar masses, from this figure we can conclude that when we have dipotassium oxalate the salting-out ability of PEGDME2000 is better than PEG2000.

**3.2. Correlation.** **3.2.1. Binodal Curve Correlation.** The binodal curves for this system are shown in Figure 1. For the correlation of binodal data of polymer + salt + water systems, several empirical equations have been proposed. All of these commonly used equations are nonlinear empirical expressions of polymer mass fraction,  $w_p$ , as a function of salt mass fraction,  $w_s$ , or vice versa and at least have three parameters. In this work for the correlation of binodal data we examined the



**Figure 4.** Binodal curves for the {PEGDME2000 (p) + K<sub>2</sub>C<sub>2</sub>O<sub>4</sub> (s) + H<sub>2</sub>O (w)}, □, and {PEG2000 (p) + K<sub>2</sub>C<sub>2</sub>O<sub>4</sub> (s) + H<sub>2</sub>O (w)}, ○, systems at: (a)  $T = 298.15$  K, (b)  $T = 318.15$  K.

performances of the temperature-dependent Merchuk equation<sup>11</sup> (eq 3) which has been successfully used previously,<sup>18</sup> the empirical equation (eq 4) that we proposed recently,<sup>6</sup> and the Graber et al.<sup>10</sup> equation with temperature dependency as given by eq 5. In these equations the temperature dependency of parameters was expressed in the linear form with  $(T - T_0)$  K as a variable.

$$w_p = [a_0 + a_1(T - T_0)] \exp([b_0 + b_1(T - T_0)]w_s^{0.5} - [c_0 + c_1(T - T_0)]w_s^3) \quad (3)$$

$$w_p = [\alpha_0 + \alpha_1(T - T_0)] + [\beta_0 + \beta_1(T - T_0)] \ln(w_s) + [\gamma_0 + \gamma_1(T - T_0)]w_s \quad (4)$$

$$1/w_s = [d_0 + d_1(T - T_0)] + [e_0 + e_1(T - T_0)]w_p^{0.5} + [f_0 + f_1(T - T_0)]w_p \quad (5)$$

In these equations,  $T$  is the absolute temperature, and  $T_0$  is assumed to be the reference temperature,  $T_0 = 273.15$  K. Also ( $a_0, a_1, b_0, b_1, c_0,$  and  $c_1$ ), ( $\alpha_0, \alpha_1, \beta_0, \beta_1, \gamma_0,$  and  $\gamma_1$ ), and ( $d_0, d_1, e_0, e_1, f_0,$  and  $f_1$ ) are independent temperature adjustable parameters of eqs 3 to 5.

The experimental binodal data at  $T = (298.15, 308.15,$  and  $318.15)$  K were fitted by nonlinear least-squares regression method to eqs 3 to 5. The fitting parameters for these equations along with the corresponding standard deviation (SD) for each temperature are given in Table 7. The standard deviations show that all of these equations can be used to reproduce the binodal data with good accuracy; however, on the basis of the obtained standard deviations, we conclude that the performance of eq 5 is better than the other equations (eqs 3 and 4). To show the reliability of these equations and the prediction ability of the locus of the binodal curves for the investigated system at temperatures where no experimental data are available, we attempted to compare the experimental polymer compositions on the binodal curve of the PEGDME2000 + K<sub>2</sub>C<sub>2</sub>O<sub>4</sub> + H<sub>2</sub>O system at  $T = 303.15$  K with those predicted using eqs 3, 4, and 5 at the corresponding temperature. On the basis of the standard deviations reported in Table 7, it can be seen that eq 5 has the best prediction ability for the temperature  $T = 303.15$  K.

**3.2.2. Tie-Line Correlation.** For the correlation of LLE data of (polymer + salt + water) systems, several models have been developed. However, in this work we decided to use the Othmer–Tobias and Bancroft<sup>12</sup> equation which is usually used to assess the reliability of experimental tie-line data, and the Setschenow-type<sup>13</sup> equation which shows good performance in the correlation and prediction of the tie-lines for such two-phase systems.

**3.2.2.1. Othmer–Tobias and Bancroft Equations.** The correlation equations given by Othmer–Tobias (eq 6a) and Bancroft<sup>12</sup> (eq 6b) have been used to correlate the tie-lines composition.

$$\left( \frac{1 - w_p^{\text{top}}}{w_p^{\text{top}}} \right) = k \left( \frac{1 - w_s^{\text{bot}}}{w_s^{\text{bot}}} \right) \quad (6a)$$

$$\left( \frac{w_w^{\text{bot}}}{w_s^{\text{bot}}} \right) = k_1 \left( \frac{w_w^{\text{top}}}{w_p^{\text{top}}} \right)^r \quad (6b)$$

where  $k, n, k_1,$  and  $r$  represented fit parameters and “top” and “bot” represent top and bottom phases, respectively. These equations have also been used to assess the reliability of LLE data. Using the tie-line data reported in Table 3, a linear dependency of the  $\log[(1 - w_p^{\text{top}})/w_p^{\text{top}}]$  plots against  $\log[(1 - w_s^{\text{bot}})/w_s^{\text{bot}}]$  and  $\log(w_w^{\text{bot}}/w_s^{\text{bot}})$  against  $\log(w_w^{\text{top}}/w_p^{\text{top}})$  is obtained, which indicated an acceptable consistency of the results. The experimental LLE data were correlated to the eq 6 using the following objective function

$$\text{OF} = \sum_T \sum_p \sum_l \sum_j (w_{T,p,l,j}^{\text{cal}} - w_{T,p,l,j}^{\text{exp}})^2 \quad (7)$$

where  $w_{T,p,l,j}$  is the mass percent of the component  $j$  in the phase  $p$  for the  $l$ th tie-line at temperature  $T$  and the superscripts “cal” and “exp” refer to the calculated and experimental values, respectively. In eq 7 the species  $j$  can be polymer, salt, or solvent molecules. The corresponding correlation coefficient values,  $R^2$ , and the values of the fitted parameters together with the deviations (Dev) are given in Table 8. On the basis of correlation coefficient values,  $R^2$ , reported in Table 8, we conclude that the reported tie-line data have acceptable consistency. Also based on the obtained deviations, we conclude that eqs 6a and 6b can be satisfactorily used to correlate the tie-line data of the investigated system.

**3.2.2.2. Setschenow-Type Equation.** The Setschenow-type equation<sup>13</sup> is a relatively simple two-parameter equation, which can be derived from the binodal theory.<sup>9</sup> The equation

**Table 7.** Values of Parameters of Equations 3, ( $a_p, b_p, c_i$ ), 4, ( $\alpha_p, \beta_p, \gamma_i$ ), and 5, ( $d_p, e_p, f_i$ ), for the PEGDME2000 + K<sub>2</sub>C<sub>2</sub>O<sub>4</sub> + Water System at  $T = (298.15, 308.15, \text{ and } 318.15)$  K

Merchuk <sup>11</sup> equation as a function of temperature (eq 3)							
T/K	$a_0$	$a_1$	$b_0$	$10^3 b_1$	$10^5 c_0$	$10^6 c_1$	SD <sup>a</sup>
	155.4164	-0.2459	-0.5644	-2.6407	2.1706	6.6515	
298.15							0.30
303.15							0.26 <sup>b</sup>
308.15							0.38
318.15							0.28
overall							0.32
empirical <sup>6</sup> equation as a function of temperature (eq 4)							
T/K	$\alpha_0$	$\alpha_1$	$\beta_0$	$\beta_1$	$\gamma_0$	$\gamma_1$	SD
	247.4697	-0.5383	-97.165	0.2067	6.0402	-0.0163	
298.15							0.15
303.15							0.08 <sup>b</sup>
308.15							0.23
318.15							0.18
overall							0.19
Graber et al. <sup>10</sup> equation as a function of temperature (eq 5)							
T/K	$d_0$	$10^3 d_1$	$10^3 e_0$	$10^3 e_1$	$10^3 f_0$	$10^4 f_1$	SD
	-0.0107	7.6394	9.0544	-3.1634	2.7082	3.8234	
298.15							0.05
303.15							0.02 <sup>b</sup>
308.15							0.08
318.15							0.05
overall							0.06

<sup>a</sup>SD =  $(\sum_{i=1}^N (100w_i^{\text{cal}} - 100w_i^{\text{exp}})^2 / N)^{0.5}$ . <sup>b</sup>Obtained from the comparison of the experimental polymer compositions,  $w_p$ , on the binodal curve of the PEGDME2000 + K<sub>2</sub>C<sub>2</sub>O<sub>4</sub> + H<sub>2</sub>O system at  $T = 303.15$  K reported in Table 2 and the corresponding data predicted using eqs 3 to 5 using the fitting parameters given in Table 7.

**Table 8.** Values of Parameters of Othmer–Tobias and Bancroft Equations, ( $K, n, k_1, r$ ), at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15)$  K, and the Steschenow Type, ( $k_p, k_s$ ) (kg·K·mol<sup>-1</sup>), Equation at  $T = (298.15, 308.15, \text{ and } 318.15)$  K for the PEGDME2000 + K<sub>2</sub>C<sub>2</sub>O<sub>4</sub> + Water System

Othmer–Tobias and Bancroft equations							
T/K	$K$	$n$	$R^2$	$k_1$	$r$	$R^2$	Dev <sup>a</sup>
298.15	0.1364	1.8698	0.9902	3.0119	0.5248	0.9860	1.08
303.15	0.1172	1.9265	0.9940	3.1317	0.5160	0.9917	0.61
308.15	0.1513	1.7552	0.9945	3.0459	0.5603	0.9914	0.58
318.15	0.1800	1.4997	0.9905	3.2477	0.6729	0.9911	0.12
Steschenow-type equation as a function of temperature							
T/K	$k_p$	$k_s \cdot 10^{-3}$	Dev				
	185.3783	1.0876					
298.15			0.02				
303.15			0.01 <sup>b</sup>				
308.15			0.04				
318.15			0.10				
overall			0.05				

<sup>a</sup>Dev =  $\sum_p \sum_l \sum_j \sum_T ((100w_{p,l,j,T}^{\text{cal}} - 100w_{p,l,j,T}^{\text{exp}})^2) / 6N$ , where  $w_{p,l,j,T}$  is the mass fraction of the component  $j$  (i.e., polymer, salt, or water) in the phase  $p$  for the  $l$ th tie-line at temperature  $T$  and  $N$  represents the number of tie-line data points. <sup>b</sup>Predicted with the corresponding model parameters obtained from the correlation of data at  $T = (298.15, 308.15, \text{ and } 318.15)$  K.

has the following form:

$$\ln \left( \frac{C_p^{\text{top}}}{C_p^{\text{bot}}} \right) = k_p + k_s (C_s^{\text{bot}} - C_s^{\text{top}}) \quad (8)$$

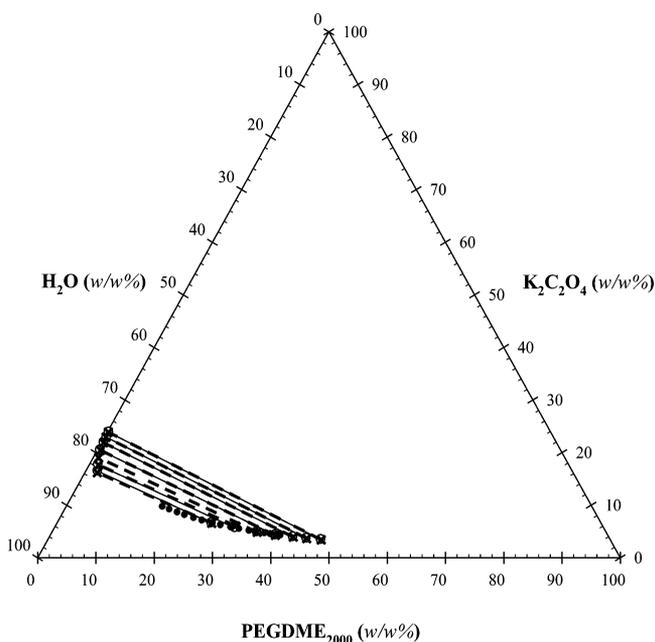
in which the  $k_s$  is the salting-out coefficient,  $k_p$  is a constant, and  $C_p$  and  $C_s$  are the molality of polymer and salt, respectively. Recently we successfully used eq 8 for the correlation of tie-line

data for the aqueous poly(propylene glycol) + potassium citrate two-phase system.<sup>19</sup> In this work, for the temperature dependency of fitting parameters of eq 8, we adopted a simple form for each parameter as follows:

$$\ln \left( \frac{C_p^{\text{top}}}{C_p^{\text{bot}}} \right) = \left[ \frac{k_p}{T} + \frac{k_s}{T} (C_s^{\text{bot}} - C_s^{\text{top}}) \right] \quad (9)$$

The parameters of eq 9 which were obtained from the correlation of the experimental LLE data at  $T = (298.15, 308.15, \text{ and } 318.15) \text{ K}$  are also given in Table 8 along with the corresponding deviations. Here, the objective function (eq 7) was also used. On the basis of deviations reported in Table 8, it is interesting to note that eq 9 with only two parameters represents the experimental LLE data with excellent accuracy for the studied system at the temperatures  $T = (298.15 \text{ to } 318.15) \text{ K}$ .

Also, for the studied system, the tie-lines at  $T = 303.15 \text{ K}$  that clearly have no contribution to obtaining the parameters,  $k_p$  and  $k_s$ , were predicted with the deviation of 0.01 in mass percent using the same parameters given in Table 8. Figure 5 shows the



**Figure 5.** Experimental and calculated tie-line data and experimental binodal data at  $T = 303.15 \text{ K}$ .  $-\circ-$ , experimental tie-lines;  $---\times---$ , calculated tie-lines from eq 9;  $\bullet$ , experimental binodal data.

experimental and the predicted tie-lines at  $T = 303.15 \text{ K}$ . On the basis of obtained deviations and from Figure 5, we conclude that eq 9 can accurately predict tie-lines at temperatures at which no experimental data are available.

**3.3. Estimated Plait Point, Slope, and the Length of Tie-Lines.** Somewhere in the binodal curve, we have a plait point where the length of tie-line has shrunk to zero, that is, when the two liquid phases become identical.<sup>20</sup> The location of the plait point for the studied system was also estimated by extrapolation from the auxiliary curve satisfactorily fitted with the following linear equation:

$$w_p = f + gw_s \quad (10)$$

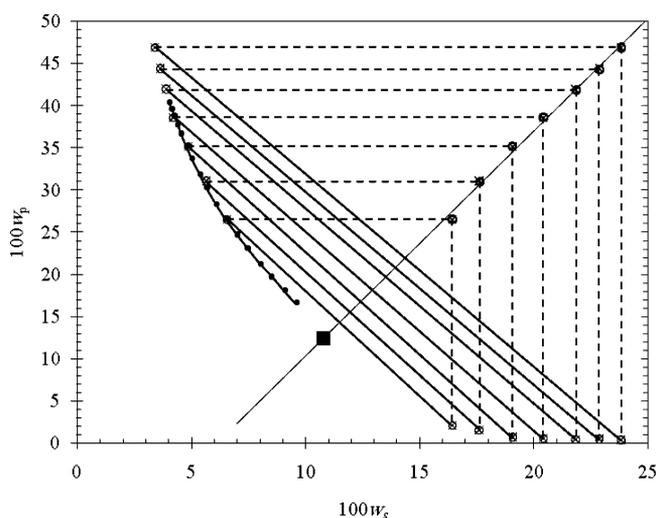
where  $f$  and  $g$  represent fit parameters. For the studied system, the estimated values for the plait points along with the obtained fitting parameters for eq 10 and the corresponding correlation coefficients,  $R^2$ , are listed in Table 9. As an example, the locus of estimated plait point for this system along with the used procedure is illustrated in Figure 6 at  $T = 303.15 \text{ K}$ .

The tie-line length, TLL, and the slope of the tie-line,  $S$ , at different compositions and temperatures were also calculated

**Table 9.** Values of Parameters of Equation 10 and the Plait Points,  $(f, g)$ , for the PEGDME2000 (p) +  $\text{K}_2\text{C}_2\text{O}_4$  (s) +  $\text{H}_2\text{O}$  (w) System at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15) \text{ K}$

$T/\text{K}$	$f$	$g$	$R^2$	plait point ( $w_p\%$ , $w_s\%$ , $w_w\%$ ) <sup>a</sup>
298.15	-14.7686	2.5062	0.9909	(13.42, 11.25, 75.33)
303.15	-16.2982	2.6657	0.9941	(12.47, 10.79, 76.74)
308.15	-11.9220	2.4280	0.9927	(12.71, 10.14, 77.15)
318.15	-3.0248	2.1945	0.9876	(15.59, 8.48, 75.93)

<sup>a</sup> $w_i$  % represents the mass percent of component  $i$ .



**Figure 6.** Binodal curve, tie-lines, and plait point for the PEGDME2000 (p) +  $\text{K}_2\text{C}_2\text{O}_4$  (s) +  $\text{H}_2\text{O}$  (w) system at  $T = 303.15 \text{ K}$ ;  $\bullet$ , experimental binodal data;  $-\circ-$ , calculated binodal from eq 5;  $\circ$ , tie-line data;  $---\times---$ , calculated auxiliary and  $\blacksquare$ , plait point.

respectively using eqs 11 and 12 as follows:

$$\text{TLL} = [(w_1^{\text{top}} - w_1^{\text{bot}})^2 + (w_2^{\text{top}} - w_2^{\text{bot}})^2]^{0.5} \quad (11)$$

$$S = (w_1^{\text{top}} - w_1^{\text{bot}})/(w_2^{\text{top}} - w_2^{\text{bot}}) \quad (12)$$

Results are also collected in Table 3.

**3.4. Free Energies of the Cloud Point (CP).** The free energy of phase separation ( $\Delta G_c$ ) can be calculated from the relation<sup>21</sup>

$$\Delta G_c = RT \ln X_p \quad (13)$$

$X_p$  is the mole fraction concentration of PEGDME at cloud point. In Table 10, the values of  $\Delta G_c$  are presented. The enthalpy values of phase separation ( $\Delta H_c$ ) were calculated by the relation,

$$\Delta H_c = \frac{d(\Delta G_c/T)}{d(1/T)} \quad (14)$$

The calculated  $\Delta H_c$  values are presented in the Table 10 which are positive and show that the aqueous two-phase formation processes are endothermic.

The following Gibbs–Helmholtz equation was used to calculate the entropy of phase separation ( $\Delta S_c$ ),

$$\Delta S_c = \frac{\Delta H_c - \Delta G_c}{T} \quad (15)$$

**Table 10.** Free Energy Changes,  $\Delta G_c$  ( $\text{kJ}\cdot\text{mol}^{-1}$ ), Entropy Changes,  $\Delta S_c$  ( $\text{J}\cdot\text{K}^{-1}\cdot\text{mol}^{-1}$ ), and Enthalpy Changes,  $\Delta H_c$  ( $\text{kJ}\cdot\text{mol}^{-1}$ ), for Clouding Point of PEGDME2000 (p) +  $\text{K}_2\text{C}_2\text{O}_4$  (s) + Water (w) for Different Salt Mass Fractions,  $w_s$ , at  $T = (298.15, 308.15, \text{ and } 318.15)$  K

$w_s$	$\Delta H_c$	T/K = 298.15		T/K = 303.15		T/K = 308.15		T/K = 318.15	
		$\Delta G_c$	$\Delta S_c$						
0.04	10.718	-12.294	77	-12.666	77	-13.040	77	-13.837	77
0.06	10.738	-13.558	81	-13.943	81	-14.301	81	-15.189	81
0.08	12.409	-14.525	90	-14.930	90	-15.318	90	-16.333	90
0.10	15.796	-15.351	105	-15.784	104	-16.247	105	-17.443	105

The calculated  $\Delta S_c$  values are all positive, and they are also collected in Table 10. This shows that the increase of entropy is the driving force for the aqueous two-phase formation processes in the studied system at  $T = (298.15, 308.15, \text{ and } 318.15)$  K.

#### 4. CONCLUSION

Liquid–liquid data for the {PEGDME2000 +  $\text{K}_2\text{C}_2\text{O}_4$  +  $\text{H}_2\text{O}$ } system were determined at  $T = (298.15, 303.15, 308.15, \text{ and } 318.15)$  K. A comparison between the experimental data shows that the phase-separation ability of the studied systems increased with increasing the temperature.

Also, from the comparison of the obtained binodal data for the {PEGDME2000 +  $\text{K}_2\text{C}_2\text{O}_4$  +  $\text{H}_2\text{O}$ } and {PEG2000 +  $\text{K}_2\text{C}_2\text{O}_4$  +  $\text{H}_2\text{O}$ } systems, we found that, for  $\text{K}_2\text{C}_2\text{O}_4$ , the phase-separation ability of PEGDME2000 is better than PEG2000. Using the Gibbs free energies of hydration of ions, the effect of type of salt on the binodals of PEGDME2000 has also been discussed.

Moreover, the experimental binodal data were satisfactorily correlated using an empirical equation and the Merchuk and the Graber et al. equations as a function of temperature with a linear temperature dependency in the form of  $(T - T_0)$  K as a variable. We found that the Graber et al. equation gives better results than the two other equations in the correlation and prediction of binodal data.

Additionally, the Othmer–Tobias and Bancroft and Setschenow-type equations were satisfactorily used for the correlation and prediction of the liquid–liquid phase behavior of the studied system. On the basis of the obtained results, it can be concluded that the Setschenow-type equation with only two parameters has a good performance in the correlation and prediction of the tie-line compositions of the studied system.

#### AUTHOR INFORMATION

##### Corresponding Author

\*Fax: +98 411 3340191. E-mail address: zafarani47@yahoo.com.

#### REFERENCES

- (1) Albertsson, P. A. *Partitioning of Cell Particles and Macromolecules*, 3rd ed.; Wiley: New York, 1986.
- (2) Walter, H.; Brooks, D. E.; Fisher, D. *Partitioning in Aqueous Two-Phase System*; Academic Press: New York, 1985.
- (3) Zaslavsky, B. Y. *Aqueous Two-Phase Partitioning, Physical Chemistry and Bioanalytical Applications*; Marcel Dekker: New York, 1995.
- (4) Zafarani-Moattar, M. T.; Nikjoo, D. Liquid-liquid and Liquid-liquid-solid Equilibrium of the Poly(ethylene glycol) dimethyl ether 2000 + Sodium Sulfate + Water System. *J. Chem. Eng. Data* **2008**, *53*, 2666–2670.

(5) Zafarani-Moattar, M. T.; Nikjoo, D. Phase Diagrams for Liquid-liquid and Liquid-solid Equilibrium of the Ternary Poly(ethylene glycol) dimethyl ether 2000 + Sodium Carbonate + Water System. *J. Chem. Eng. Data* **2009**, *54*, 2918–2922.

(6) Zafarani-Moattar, M. T.; Nemati-Kande, E. Study of Liquid-liquid and Liquid-solid Equilibria of the Ternary Aqueous System Containing Poly(ethylene glycol) dimethyl ether 2000 and Tri-potassium Phosphate at different Temperatures: Experiment and Correlation. *CALPHAD: Comput. Coupling Phase Diagrams Thermochem.* **2010**, *34*, 478–486.

(7) Zafarani-Moattar, M. T.; Nasiri, S. (Liquid + liquid) and (Liquid + solid) Equilibrium of Aqueous Two-Phase Systems Containing polyethylene glycol di-methyl ether 2000 and Di-sodium Hydrogen Phosphate. *J. Chem. Thermodyn.* **2010**, *42*, 1071–1078.

(8) Zafarani-Moattar, M. T.; Nemati-Kande, E. Thermodynamic Studies on the Complete Phase Diagram of Aqueous Two Phase System Containing Polyethylene glycol dimethyl ether 2000 and Di-potassium Hydrogen Phosphate at different Temperatures. *CALPHAD: Comput. Coupling Phase Diagrams Thermochem.* **2011**, *35*, 165–172.

(9) Guan, Y.; Lilley, T. H.; Treffry, T. E. A New Excluded Volume Theory and Its Application to the Coexistence Curves of Aqueous Polymer Two-Phase System. *Macromolecules* **1993**, *26*, 3971–3979.

(10) Graber, T. A.; Taboada, M. E.; Cartón, A.; Bolado, S. Liquid-liquid Equilibria of the Poly(ethylene glycol) + Sodium Nitrate + Water Systems at 298.15 K. *J. Chem. Eng. Data* **2000**, *45*, 182–184.

(11) Merchuk, J. C.; Andrews, B. A.; Asenjo, J. A. Aqueous Two-Phase Systems for Protein Separation: Studies on Phase Inversion. *J. Chromatogr., B* **1998**, *711*, 285–293.

(12) Othmer, D. F.; Tobias, P. E. Liquid-liquid Extraction Data-toluene and Acetaldehyde Systems. *Ind. Eng. Chem.* **1942**, *34*, 690–692.

(13) Hey, M. J.; Jackson, D. P.; Yan, H. The Salting-out Effect and Phase Separation in Aqueous Solutions of Electrolytes and Poly(ethylene glycol). *Polymer* **2005**, *46*, 2567–2572.

(14) Cheluget, E. L.; Gelinás, S.; Vera, J. H.; Weber, M. E. Liquid-liquid Equilibrium of Aqueous Mixtures Poly(propylene glycol) with NaCl. *J. Chem. Eng. Data* **1994**, *39*, 127–130.

(15) Hartounian, H.; Floeter, E.; Kaler, E. W.; Sandler, S. I. Effect of Temperature on the Phase Equilibrium of Aqueous Two-Phase Polymer System. *AIChE J.* **1993**, *39*, 1976–1984.

(16) Marcus, Y. Thermodynamics of Solvation of Ions: Part 5. Gibbs Free Energy of Hydration at 298.15 K. *J. Chem. Soc., Faraday Trans.* **1991**, *87*, 2995–2999.

(17) Zafarani-Moattar, M. T.; Zaferanloo, A. Measurement and Correlation of Phase Equilibria in Aqueous Two-Phase Systems Containing Polyvinylpyrrolidone and Di-potassium Tartrate or Di-potassium Oxalate at different Temperatures. *J. Chem. Thermodyn.* **2009**, *41*, 864–871.

(18) Zafarani-Moattar, M. T.; Hamzehzadeh, S. Diagrams for the Aqueous Two-Phase Ternary System Containing the Ionic Liquid 1-Butyl-3-Methylimidazolium Bromide and Tri-potassium Citrate at  $T = (278.15, 298.15 \text{ and } 318.15)$  K. *J. Chem. Eng. Data* **2009**, *54*, 833–841.

(19) Zafarani-Moattar, M. T.; Emamian, S.; Hamzehzadeh, S. Effect of Temperature on the Phase Equilibrium of the Aqueous Two-Phase Poly(propylene glycol) + Tri-potassium Citrate System. *J. Chem. Eng. Data* **2008**, *53*, 456–461.

(20) Lee, B. H.; Qin, Y.; Prausnitz, J. M. Thermodynamic Representation of Ternary Liquid–liquid Equilibria near-to and far-from the Plait point. *Fluid Phase Equilib.* **2006**, *240*, 67–72.

(21) Dan, A.; Ghosh, S.; Moulik, S. P. The Solution Behavior of Poly(vinylpyrrolidone): Its Clouding in Salt Solution, Solvation by Water and Isopropanol, and Interaction with Sodium Dodecyl Sulfate. *J. Phys. Chem. B* **2008**, *112*, 3617–3624.